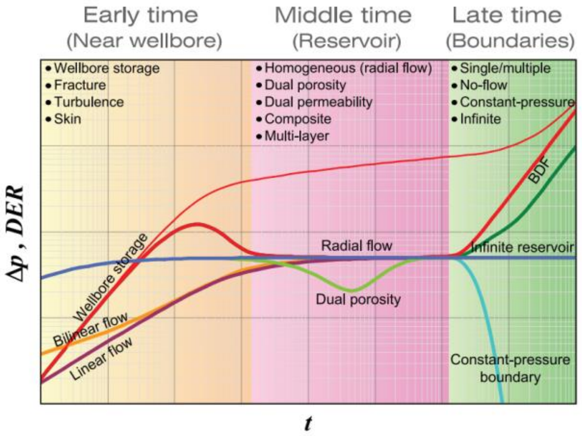
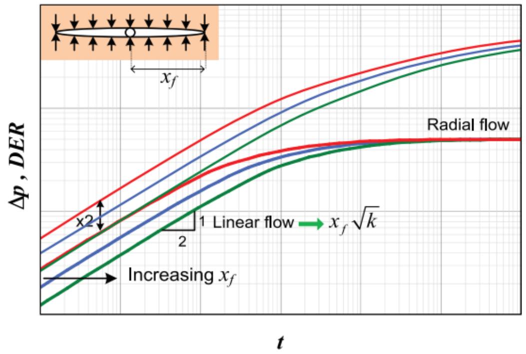
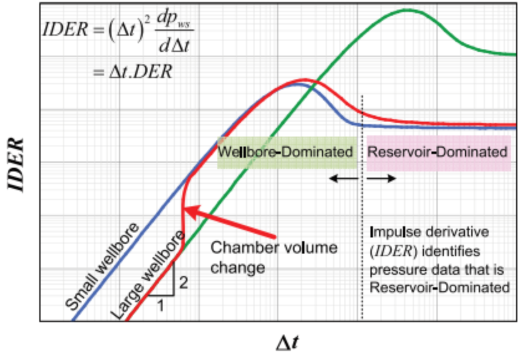
Well Testing Fundamentals



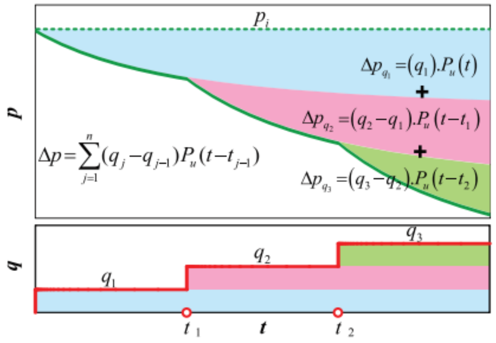
Reservoir Linear Flow (Fracture) – Half Slope



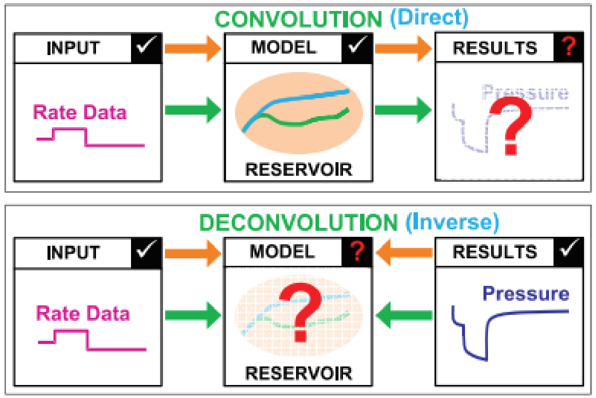
Impulse Derivative (IDER)

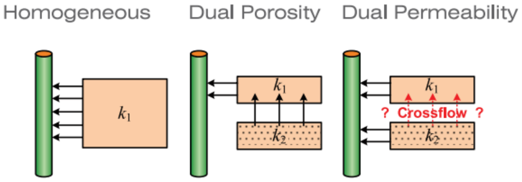


Superposition-in-Time



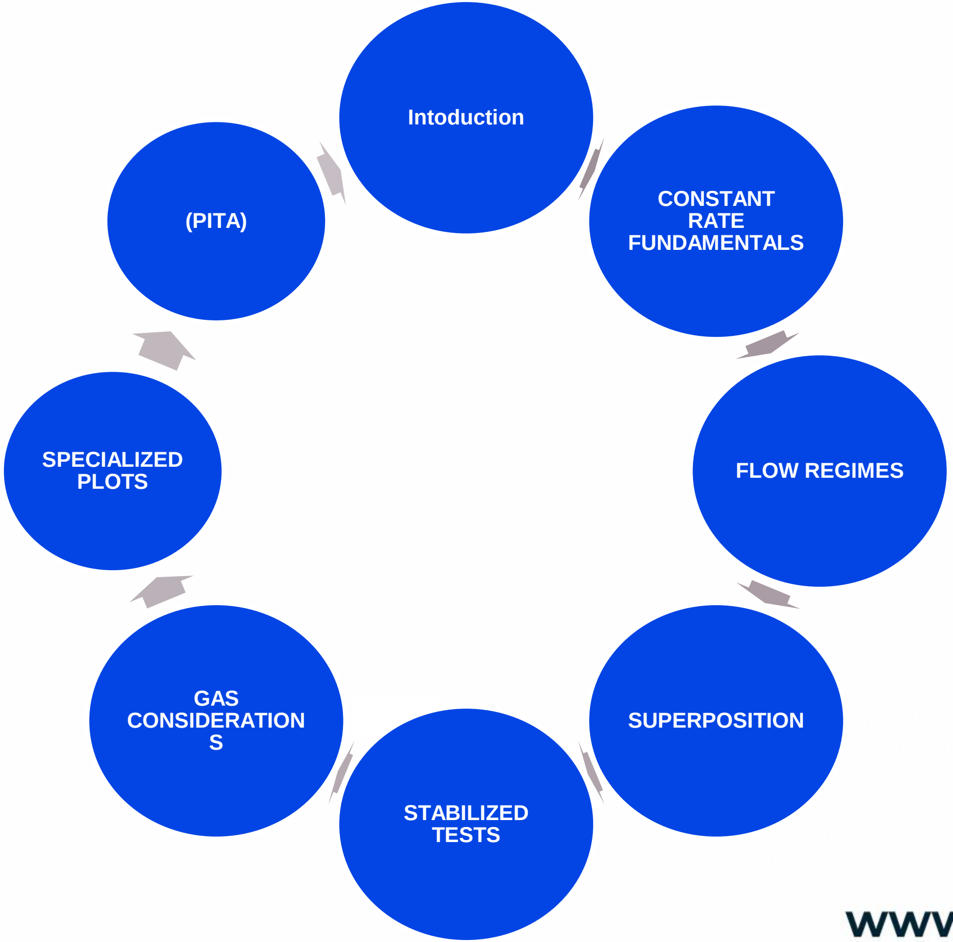
Direct and Inverse Processes





- **Dual Porosity:** Only porosity 1 is connected to the well, and porosity 2 acts like a source. Example: naturally fractured reservoir: fissures (1); matrix (2)
- **Dual Permeability:** Each porosity is connected to the well. Example: two layers commingled at the well. Crossflow in the reservoir may or may not exist

Agenda



Intoduction
CONSTANT RATE FUNDAMENTALS
FLOW REGIMES
SUPERPOSITION
STABILIZED TESTS
GAS CONSIDERATION S
SPECIALIZED PLOTS
(PITA)

Introduction

What is a test?

Measurement of rate, time and pressure under controlled conditions.

Why test?

- Reservoir pressure
- Permeability
- Wellbore damage
- Deliverability
- Reservoir management
- Reservoir description
- Fluid samples
- Regulations

+ Well testing theory is based on constant rate Drawdown tests. Drawdown tests are not very practical (due to poor data quality). Buildup tests are more common.

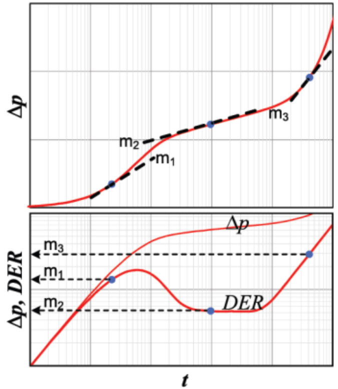
Transient Tests →	**Reservoir Characterization**
RFT®, WFT®, MDT® …	p_i, k, fluid samples
DST	p_i, k, fluid samples
Drawdown+ / Injection	k, s (often un-interpretable)
Buildup+ / Falloff	k, s, $\overline{p}_R$
Interference/Pulse	k, ϕc_t, lateral/vertical continuity
PITA, PID, Minifrac, CCT	p_i, k
Stabilized Tests →	**Deliverability Forecasting**
IPR	q_{stab}
AOF	q_{stab}

Derivative

- Derivative (DER) is the slope of the semilog plot.

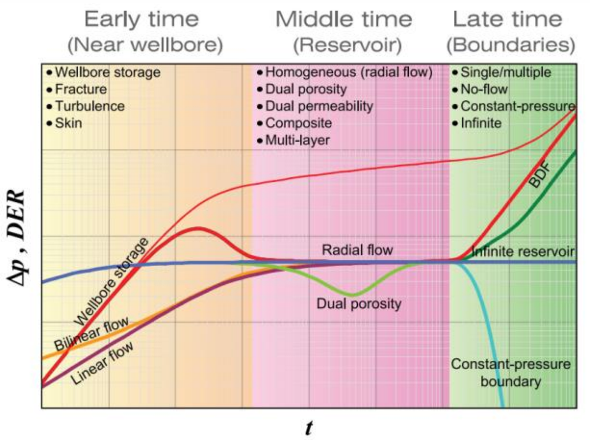
$$DER = \frac{d\Delta p}{d\ln t} = t\frac{d\Delta p}{dt}$$

- *DER* is usually plotted on log-log coordinates, combined with a plot of Δp.
- *DER* is used for flow regime diagnostics.

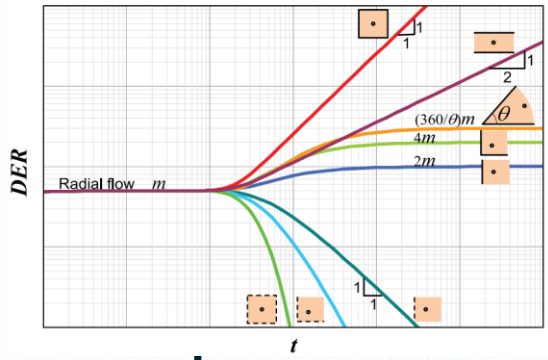


CONSTANT RATE FUNDAMENTALS

Flow regime		Derivative Slope	Time Function*	Result
Wellbore storage		1	t	C, C_D
Bilinear flow		1/4	$\sqrt[4]{t}$	$k^{1/4}\sqrt{k_f w}$
Linear flow	fracture	1/2	$\sqrt{t}$	$x_f\sqrt{k}$
	horiz. well			$L_e\sqrt{k_y}$
Spherical flow		-1/2	$1/\sqrt{t}$	$\sqrt[3]{k_x k_y k_z}$
Vertical radial flow in horizontal wells		0	$\log(t)$	$L_e\sqrt{k_y k_z}$
Radial flow (∞-acting)		0	$\log(t)$	kh
Linear flow – Channel		1/2	$\sqrt{t}$	$W\sqrt{k}$
Boundary-Dominated Flow		1	t	V_p



Boundaries



FLOW REGIMES - STORAGE

Storage Flow Regime is equivalent to emptying a tank

$$c = \frac{-1}{V}\frac{\Delta V}{\Delta p} = \frac{-1}{V}\frac{qt}{\Delta p}$$

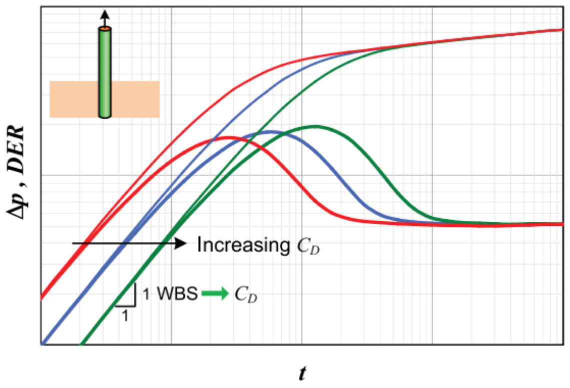
Early time: Wellbore Storage (WBS)

- Pressure and derivative have unit slope

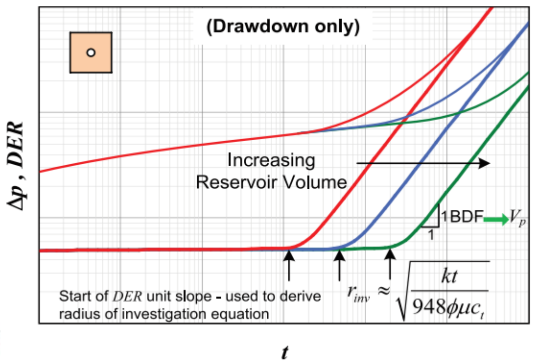
Late time: Boundary-Dominated Flow (BDF)

- Also known as:
  - Pseudo-steady state
  - Stabilized
  - Tank-type behavior
- Applies to Drawdown only – **NOT Buildup**
- Derivative unit slope occurs much earlier than pressure unit slope

Wellbore Storage - Unit Slope



Reservoir Storage (BDF) - Unit Slope



FLOW REGIMES - LINEAR FLOW

Early Time → fracture

- Infinite conductivity fracture
- Pressure and derivative have slope of ½ (Separated by a factor of 2)
- Equivalent to negative skin

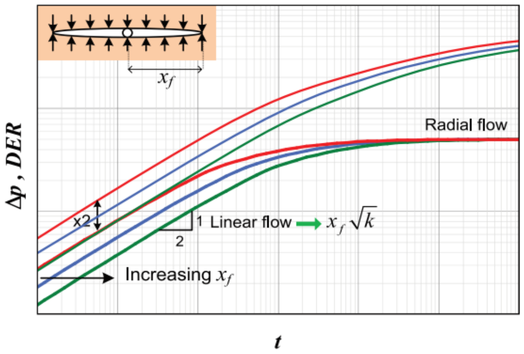
$$r_{wa} = \frac{x_f}{2} \Rightarrow s = \ln\left(\frac{2r_w}{x_f}\right)$$

- Fracture effectiveness may be reduced by:
  - Skin on fracture face
  - Choke skin
  - Finite conductivity within the fracture

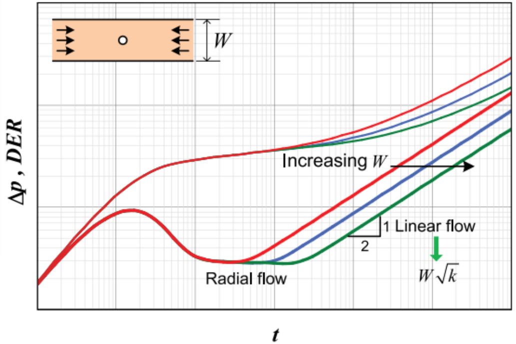
Late Time → channel (parallel boundaries)

- Derivative has slope of ½

Reservoir Linear Flow (Fracture) – Half Slope



Reservoir Linear Flow (Channel) – Half Slope

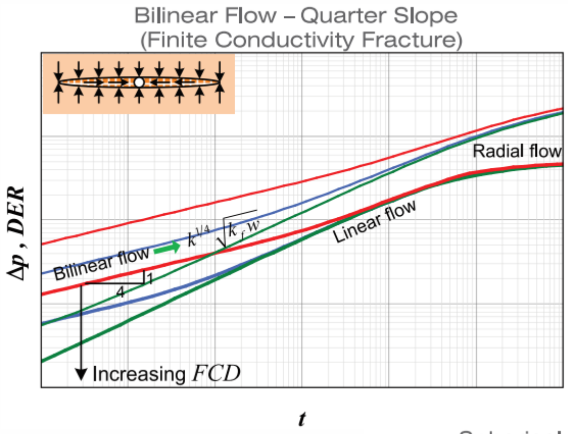


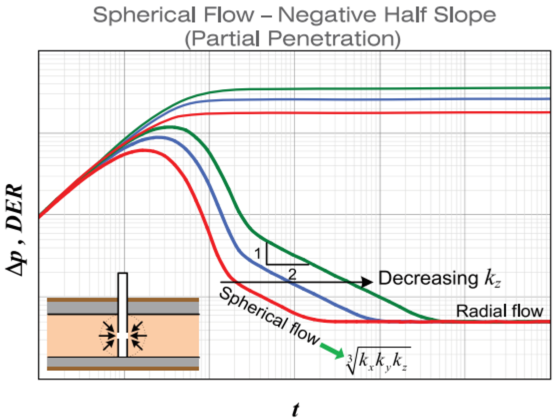
FLOW REGIMES - BILINEAR FLOW

- Finite conductivity fracture
- Dimensionless Fracture Conductivity $FCD = \frac{k_f w}{k x_f}$
- Bilinear flow regime precedes linear flow
- $FCD > 100$ ➞ infinite conductivity fracture

SPHERICAL FLOW

- Partial Penetration or limited perforations
- Slope of derivative is -½
- Component of total skin
- Magnitude of skin depends on vertical permeability and perforation interval
- Radial flow from completed interval may be observed before spherical flow



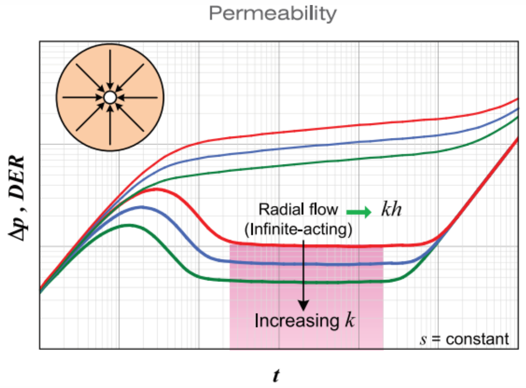


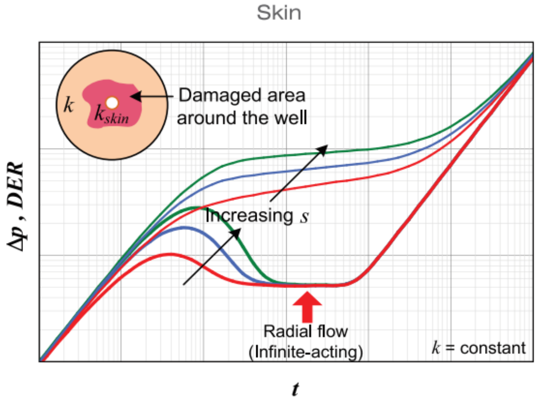
FLOW REGIMES - RADIAL FLOW

- Derivative has a slope of zero
- Used to obtain permeability

SKIN

- $\Delta p|_{skin}$ = difference between ideal and measured flowing pressure
- $s = \Delta p|_{skin}$ expressed in dimensionless form
- Skin $s = \left(\frac{k}{k_{skin}} - 1\right) \ln \frac{r_{skin}}{r_w}$
- Apparent wellbore radius $r_{wa} = r_w e^{-s}; \quad s = \ln \frac{r_w}{r_{wa}}$
- Total skin, $s' = s_{damage} + s_{turbulence} + s_{partial\ penetration} + s_{geometry} + s_{fracture} + \ldots$

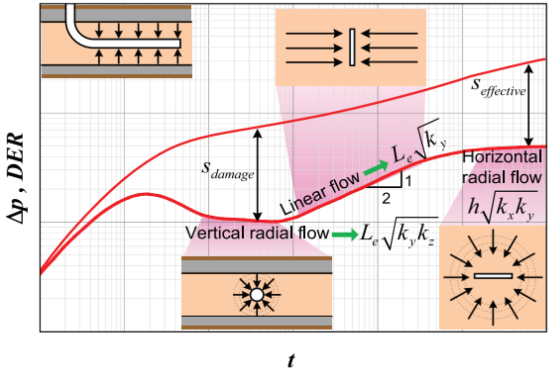




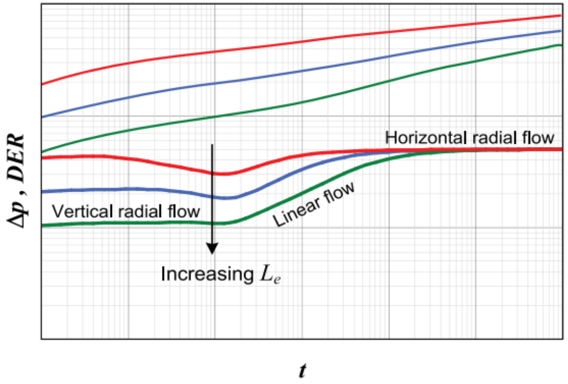
HORIZONTAL WELL FLOW REGIMES

- Vertical radial flow → vertical permeability, $\sqrt{k_y k_z}$ skin around wellbore, s_{damage}
- Linear flow → k_y or effective wellbore length, L_e
- Once linear flow is reached, horizontal well is similar to vertical fractured well + $s_{convergence}$
- Horizontal radial flow → horizontal permeability, $\sqrt{k_x k_y}$, and skin equivalent to vertical well, $s_{effective}$

Horizontal Well



Effective Well Length



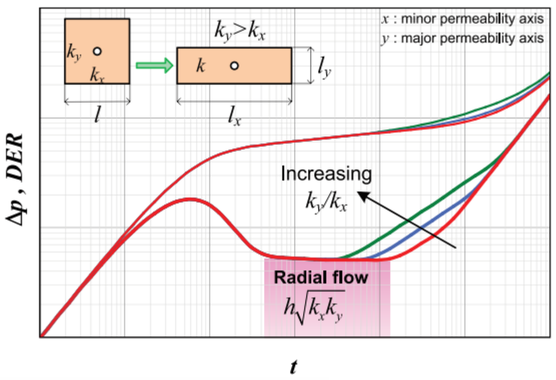
ANISOTROPY

- Anisotropy affects the drainage pattern
- It creates elliptical iso-potentials
- Coordinate transformation converts anisotropic reservoir models to equivalent isotropic ones of different dimensions

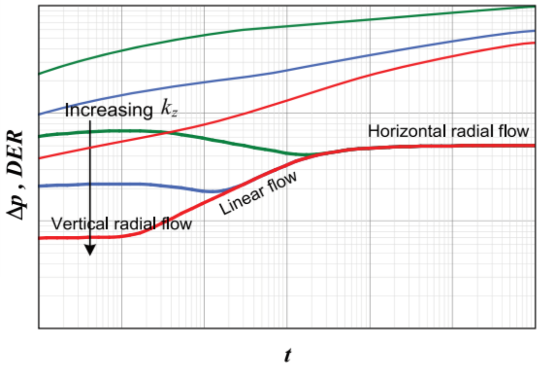
$$l_x = l\sqrt{k/k_x} \qquad k = \sqrt{k_x k_y}$$
$$l_y = l\sqrt{k/k_y}$$

- Horizontal anisotropy is important in certain depositional environments; such as naturally fractured reservoirs or coals
- Vertical anisotropy is common and affects skin whenever there is flow in the vertical direction, such as partial penetration

Vertical Well - Horizontal Anisotropy



Horizontal Well - Vertical Anisotropy



DUAL POROSITY / PERMEABILITY

- Storativity ratio (ω) gives an indication of the fraction of the hydrocarbons stored in the fissures (porosity 1)

$$\omega = \frac{(\phi c_t h)_1}{(\phi c_t h)_1 + (\phi c_t h)_2}$$, typically 0.01 to 0.1

- Interporosity Flow Coefficient (λ) reflects the contrast between matrix and fracture permeability; it also depends on matrix size and geometry

$$\lambda = \alpha \frac{k_2}{k_1}$$, typically 10^{-4} to 10^{-8}

- α is a shape factor that depends on the size and geometry of the matrix

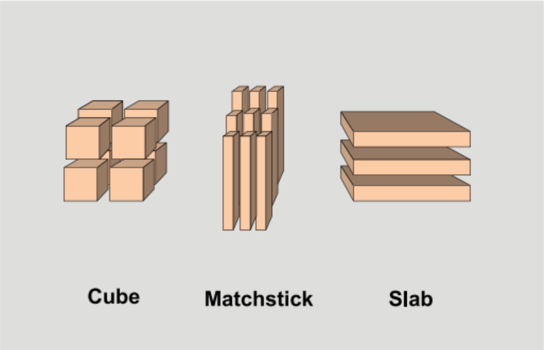
- $\lambda = 0$ → No crossflow in the reservoir

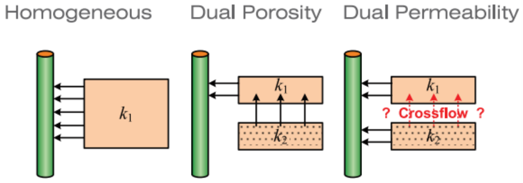
- Flow Capacity Ratio (κ) is the contribution of the high permeability layer with respect to the total

$$\kappa = \frac{k_1 h_1}{k_1 h_1 + k_2 h_2}$$

- $k_2 \to 0, \ \kappa \approx 1$ → dual porosity

Matrix Element Shapes





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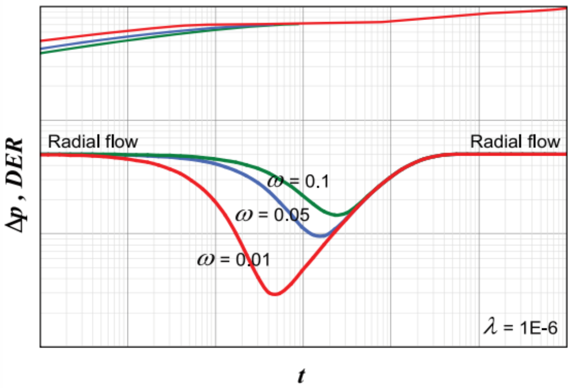
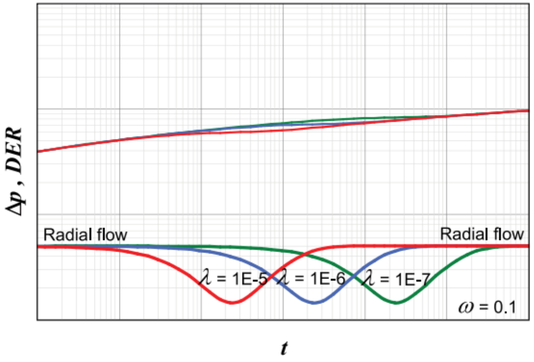
Effect of Omega (ω)



Effect of Lambda (λ)



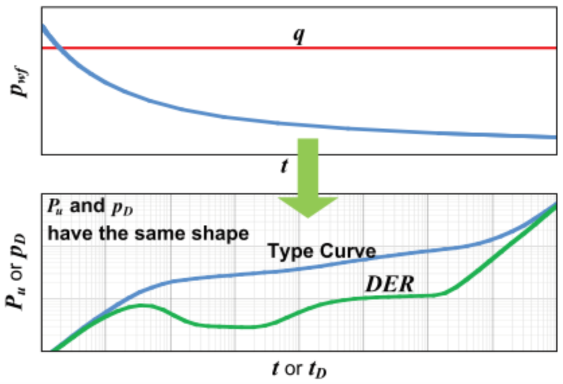
SUPERPOSITION - UNIT RATE FUNCTION

- Unit Rate Function, P_u, is defined as the pressure drop per unit constant flow rate : $P_u = (\Delta p / q)$
- It is the fundamental solution of the Diffusivity Equation used in Well Test Interpretation
- P_u is often expressed in dimensionless form

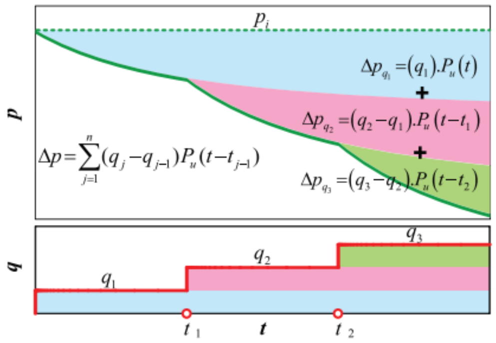
$$p_D = \frac{\Delta p k h}{141.2 q B \mu} \qquad t_D = \frac{2.637E-4\ kt}{\phi \mu c_t r_w^2}$$

- It is called a Type Curve when plotted on log-log coordinates, and is usually presented with the semilog derivative $DER = d(p_D) / d(\ln t_D)$
- Every reservoir has its own Unit Rate Function; the shape of its derivative reflects the reservoir model

Unit Rate Function



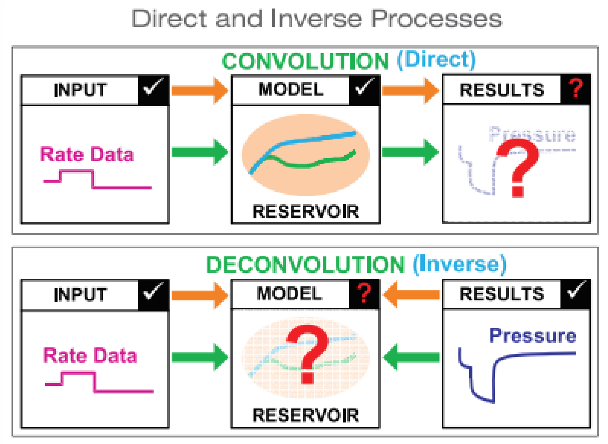
Superposition-in-Time

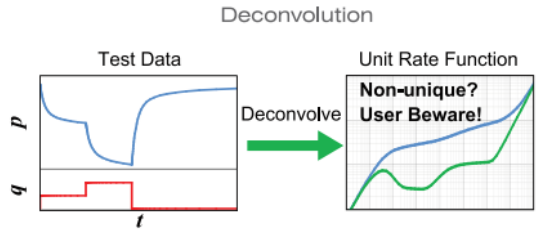


SUPERPOSITION - DECONVOLUTION

DECONVOLUTION

- Deconvolution is the reverse of superposition
- Its purpose is to extract the Unit Rate Function from pressure data in multi-rate tests
- This Unit Rate Function is in fact the reservoir Type Curve; it facilitates identification of the reservoir model
- It does NOT require a pre-conceived reservoir model; rather, it is used to determine what the reservoir model might be
- It is used to convert buildup or multi-rate data into the corresponding constant rate Drawdown Type Curve





Limitations

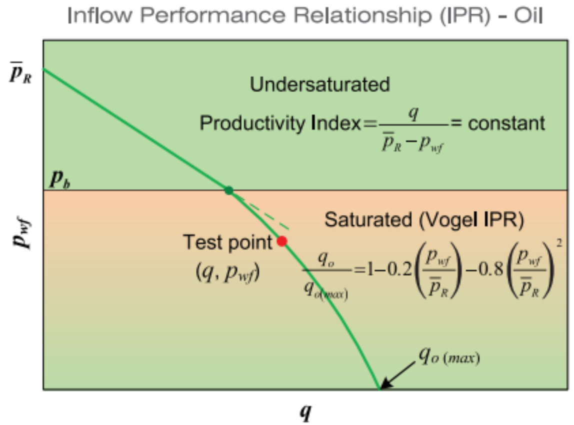
- Very sensitive to data quality
- Changing skin, changing wellbore storage, missing/ incorrect initial pressure and gaps in data can have a significant effect on the shape of the deconvolved Type Curve

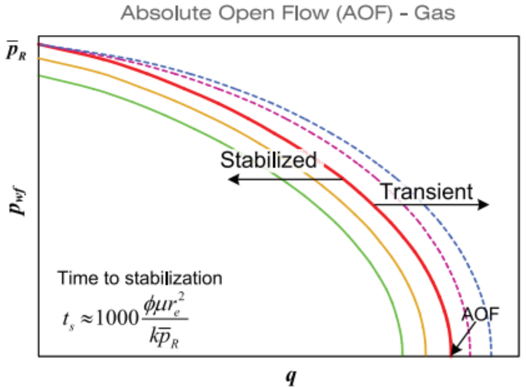
STABILIZED TESTS

IPR FOR OIL .... AOF FOR GAS

Deliverability Tests : Evaluate deliverability, **NOT** reservoir characteristics

- **IPR :** Inflow Performance Relationship
  - Flow potential of a well at any sandface pressure
  - Single point test
- **AOF :** Absolute Open Flow
  - Maximum rate of a gas well when back pressure at sandface is zero
  - Multiple rates required to evaluate turbulence



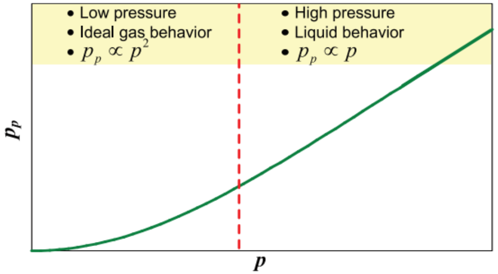


GAS CONSIDERATIONS
PSEUDO-PRESSURE (Pp)

- Welltest equations are based on liquid flow equations:
  - Constant μ
  - Constant c
- Gas properties (μ, c and Z) vary with pressure
- Pseudo-pressure accounts for variations of μ and Z
- Pseudo-pressure is an **exact** transformation
- Replacing p by p_p makes Darcy's Law applicable to gas (when expressed in terms of flow rate at standard conditions)
- p_p does **NOT** account for variation in gas compressibility (c_g) with pressure (see pseudo-time)

Pseudo-Pressure

$$p_p = 2\int_{p_0}^{p} \frac{p\,dp}{\mu Z}$$



Gas: Replace (pressure p → pseudo-pressure p_p; time t → pseudo-time t_a)

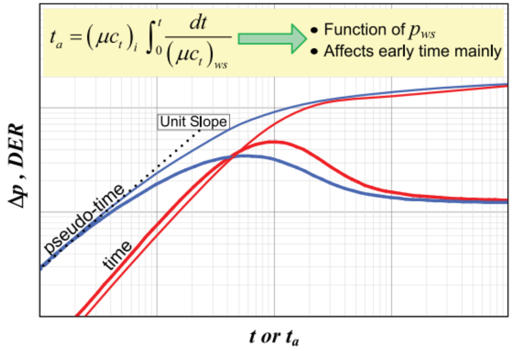
	Liquid	Gas
p_D	$(p_i - p_{wf})\dfrac{kh}{141.2qB\mu}$	$(p_{p\,i} - p_{p\,wf})\dfrac{kh}{1.417E6qT}$
t_D	$\dfrac{0.0002637kt}{\phi\mu c_t r_w^2}$	$\dfrac{0.0002637kt_a}{\phi(\mu c_t)_i r_w^2}$
c_t	constant $S_{gi}c_{gi} + S_{oi}c_{oi} + S_{wi}c_{wi} + c_f$	Varies with pressure $S_g c_g + S_o c_o + S_w c_w + c_f + c_d^{**}$

**CBM desorption compressibility, $c_d = \dfrac{\rho_B B_g V_L}{\phi}\dfrac{p_L}{(p_L + p)^2}$

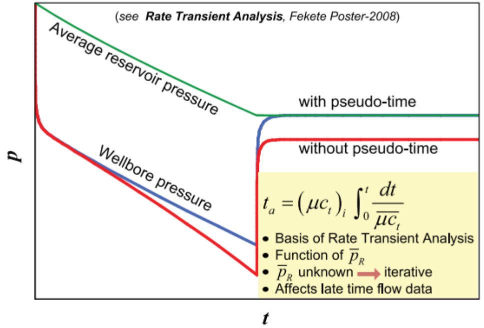
GAS CONSIDERATIONS PSEUDO-TIME (ta)

- Pseudo-time (t_a) corrects for variation of gas viscosity (μ_g) and compressibility (c_g) with pressure
- At low pressure c_g varies significantly ➡ $c_g \approx \frac{1}{p}$
- Pseudo-time transformation is **not exact**
- Pseudo-time is defined **DIFFERENTLY** for drawdown and buildup
    - In well testing (buildup analysis) pseudo-time is defined in terms of pressure at the **wellbore**
    - For analysis of production data (long drawdowns) pseudo-time is defined in terms of the **average reservoir pressure** NOT the wellbore pressure

Buildup Pseudo-Time



Drawdown Pseudo-Time



GAS CONSIDERATIONS - TURBULENCE (HIGH VELOCITY NON-DARCY FLOW)

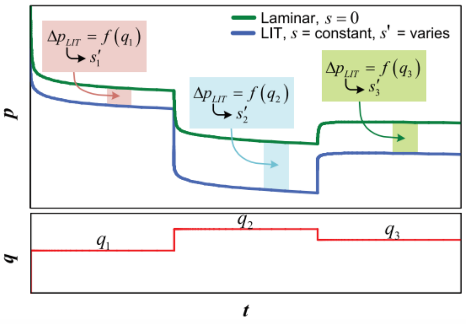
- Gas flow within the reservoir can be laminar or turbulent
- Velocity increases as the wellbore is approached
- Turbulence near the wellbore area causes an additional pressure drop that is treated as skin
- Skin due to turbulence is rate-dependent
- Multiple rates are required to quantify turbulence
- Positive skin usually means damage; however it could represent a stimulated well with turbulence

LAMINAR-INERTIAL-TURBULENT (LIT) FLOW

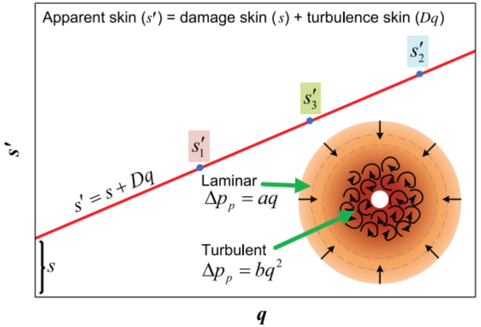
(Forchheimer or Houpeurt Equation)

$\Delta p_p = aq + bq^2$ or sometimes $\Delta p^2 \approx a'q + b'q^2$

Pressure Drop due to Turbulence



Turbulence Factor D

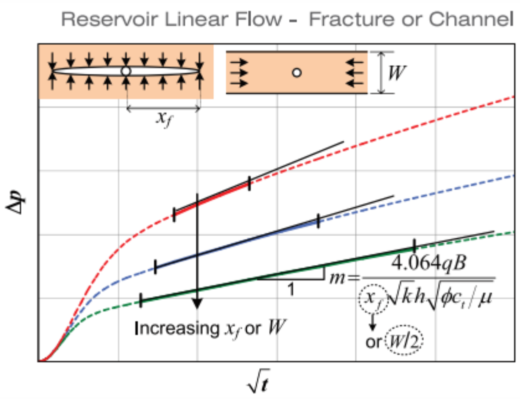


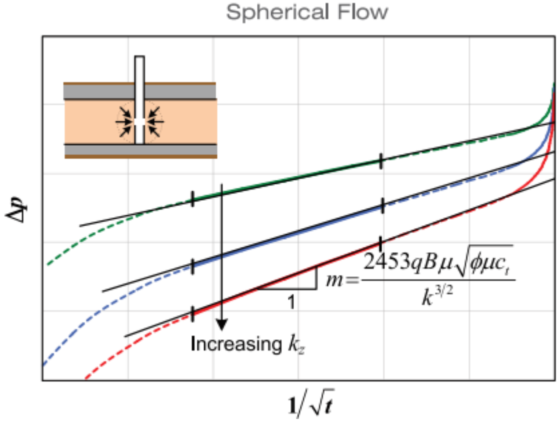
SPECIALIZED PLOTS

- A specialized plot is a plot of the pressure data on a time axis that is specific to a particular flow regime:

Flow Regime	X-Axis
Radial flow (horizontal)	$\log(t)$
Radial flow (vertical)	$\log(t)$
Linear flow (fracture)	$\sqrt{t}$
Linear flow (channel)	$\sqrt{t}$
Bilinear flow	$\sqrt[4]{t}$
Spherical flow	$1/\sqrt{t}$
Wellbore storage (afterflow)	t
Boundary-dominated flow	t

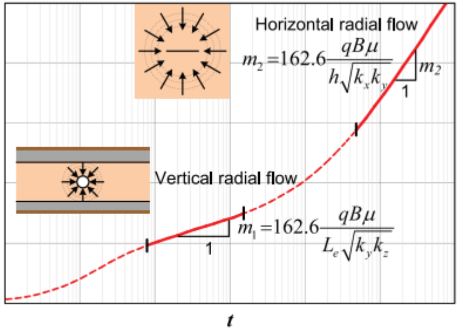
- It exhibits a straight line during that flow regime
- The slope of the line gives the result of interest



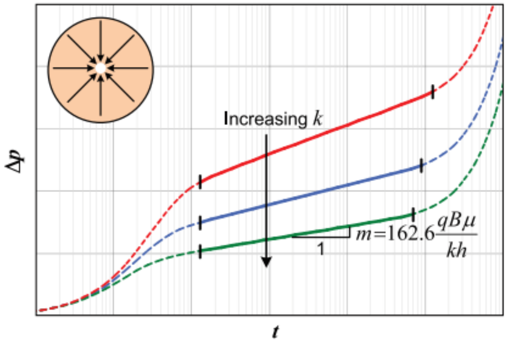


SPECIALIZED PLOTS

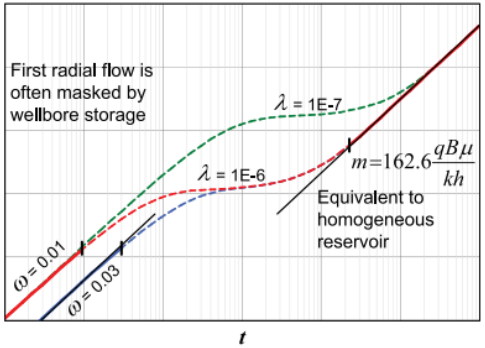
Radial Flow - Horizontal Well



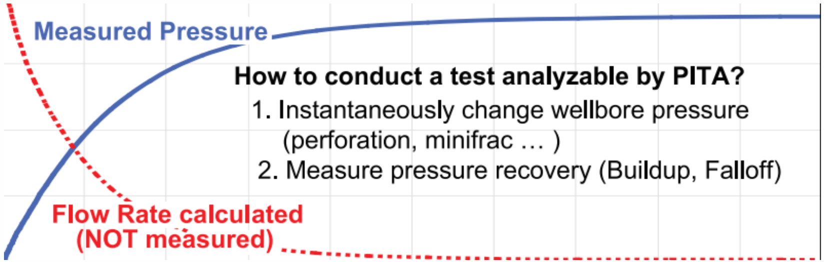
Radial Flow

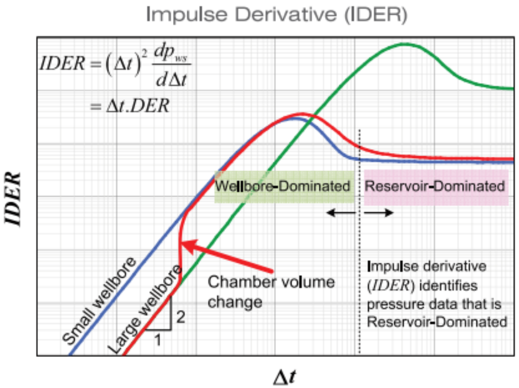


Radial Flow - Dual Porosity

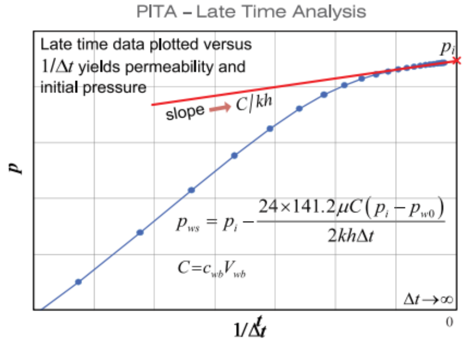


PERFORATION INFLOW TEST ANALYSIS (PITA)





- Pre-frac test
- Useful for determining initial pressure and permeability of low permeability reservoirs
- PITA is similar to other tests:
  Slug, Surge®, Impulse®, Perforation Inflow Diagnostic (PID), Closed Chamber Test (CCT), Flow Rate Tester (FRT®), DFIT®, Minifrac, After-Closure-Analysis (ACA), ...



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